

# An experimental determination of W, Nb, and Ta partition coefficients between P-rich peraluminous granitic melt and coexisting aqueous fluid

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**Abstract** The partition coefficients of W, Nb, and Ta between the P-rich peraluminous granitic melt and the coexisting aqueous fluid were determined at 800–850 °C and 0.5–1.5 kbar. The experimental results showed that the partition coefficients  $D_W$ ,  $D_{Nb}$ , and  $D_{Ta}$  ( $D_i^{y/m} = C_i^y/C_i^m$ , where  $C_i^y$  and  $C_i^m$  denote the concentrations of an element,  $i$ , in the aqueous fluid and the melt, respectively) were less than 0.1. All partition coefficients were affected by pressure, but there was no evidence for the complexation of  $P_2O_5$  with these elements in the granitic melt or aqueous fluid, except for with W in the fluid. The results showed that W, Nb, and Ta tended to partition into the granitic melt and, in the late period of crystallization of P-rich magma, they formed independent minerals.

**Keywords** Partition coefficient · P-rich granitic melt · Fluid

## 1 Introduction

Some peraluminous granites, pegmatites, and rhyolites—particularly those with S-type affinity—are enriched in phosphorus. Whole-rock values of >1 wt%  $P_2O_5$  have been reported for certain granites (Raimbault et al. 1995; Lentz 1997; London 1998; Raimbault and Buroil 1998; Zhang 2001).

Extremely high concentrations of phosphorus in evolved granitic melts lead to the crystallization of amblygonite-montebrazite  $LiAlPO_4(F,OH)$ , ithiophyllite-triphyllite  $Li(Mn,Fe)PO_4$  (London 1987), and/or ferromagnesian phosphate minerals including childernite-eosphorite series phases and sarcopside (London et al. 1999). Although the effect of phosphorus on the viscosity of granitic melts and the solubility of water in granitic melts appears to be small, compared with F or B (Dingwell et al. 1993; Holtz et al. 1993; Toplis and Dingwell 1996), experimental studies have shown that phosphorus can lower the solidus temperatures of granitic melts and can expand the liquidus field of quartz, ultimately leading to the formation of peralkaline, silicate-poor residual melts (Wyllie and Tuttle 1964; London et al. 1993). Rare-element ore deposits mineralized with W, Nb, and Ta are closely associated with the P-rich peraluminous igneous rocks spatially and temporally (e.g., Baxiannao tungsten deposit, Yichun 414 Nb–Ta deposit, Nanping No. 3 pegmatite, and Beauvoir granite) (Huang et al. 2002; Li et al. 2010; Raimbault et al. 1995; Yang et al. 1994), but the effect of phosphorus on the vapor/melt partitioning behavior of W, Nb and Ta is still not known in detail. The purpose of this study is to investigate the partitioning of these elements and phosphorus's role in the partitioning of these ore metals in magmatic-hydrothermal systems.

## 2 Experimental methods

### 2.1 Starting materials

An albite granite, termed YS-02-48 from the Yichun 414 pluton, was the starting material (Table 1). A small block of the albite granite was cleaned in distilled water, dried, then ground in an agate mortar until it was less than 200 mesh in grain size. To meet the analytical accuracy

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**Table 1** Compositions of the sample and starting glass versus Macusanite and Ongonite (wt%)

| Sample                         | YS-02-48 | Macusanite <sup>a</sup> | Ongonite <sup>a</sup> | P0T   | P2T   | P5T   | P8T   |
|--------------------------------|----------|-------------------------|-----------------------|-------|-------|-------|-------|
| SiO <sub>2</sub>               | 73.82    | 72.32                   | 72.47                 | 74.16 | 72.86 | 70.79 | 68.06 |
| TiO <sub>2</sub>               | 0.02     | 0.02                    | 0.00                  | 0.02  | 0.02  | 0.02  | 0.01  |
| Al <sub>2</sub> O <sub>3</sub> | 15.17    | 15.63                   | 16.66                 | 15.56 | 15.21 | 14.75 | 14.39 |
| Fe <sub>2</sub> O <sub>3</sub> | 0.32     | 0.52 <sup>b</sup>       | 0.52 <sup>b</sup>     | 0.41  | 0.40  | 0.40  | 0.41  |
| MnO                            | 0.09     | 0.06                    | 0.11                  | 0.09  | 0.09  | 0.09  | 0.09  |
| MgO                            | 0.02     | 0.00                    | 0.25                  | 0.19  | 0.2   | 0.19  | 0.44  |
| CaO                            | 0.49     | 0.23                    | 0.18                  | 0.33  | 0.33  | 0.32  | 0.43  |
| Na <sub>2</sub> O              | 5.12     | 4.10                    | 4.65                  | 5.24  | 5.13  | 4.97  | 4.95  |
| K <sub>2</sub> O               | 3.42     | 3.53                    | 3.13                  | 3.61  | 3.52  | 3.40  | 3.28  |
| P <sub>2</sub> O <sub>5</sub>  | 0.32     | 0.58                    | /                     | 0.27  | 1.91  | 4.83  | 7.71  |
| F                              | 0.23     | 1.31                    | 1.09                  | /     | /     | /     | /     |
| B <sub>2</sub> O <sub>3</sub>  | 0.02     | 0.62                    | /                     | /     | /     | /     | /     |
| H <sub>2</sub> O               | 0.74     | 0.30                    | 0.98                  | /     | /     | /     | /     |
| total                          | 99.69    | 99.78                   | 100.43                | 99.87 | 99.66 | 99.74 | 99.75 |
| <sup>a</sup> ASI               | 1.17     | 1.42                    | 1.47                  | 1.19  | 1.18  | 1.19  | 1.16  |
| <sup>a</sup> W <sup>b</sup>    |          |                         |                       | 428   | 485   | 505   | 541   |
| <sup>b</sup> Nb <sup>b</sup>   |          |                         |                       | 221   | 229   | 278   | 423   |
| <sup>b</sup> Ta <sup>b</sup>   |          |                         |                       | 198   | 216   | 202   | 247   |

<sup>a</sup> Datas from London et al. (1989)

<sup>b</sup> The total Fe as FeO, / not determined (these elements are in ppm)

requirements of trace elements in experimentally run-products, glass and aqueous fluid by LA-ICPMS and solution ICP-MS, certain concentrations, e.g., 500 ppm W, 200 ppm Nb and, 200 ppm Ta, together with various concentrations of phosphorus, were doped in the initial material during the glasses preparation by using a silicon-molybdenum electric furnace. Phosphorus in the initial glass was added in the form of (NH<sub>4</sub>)H<sub>2</sub>PO<sub>4</sub>, and trace elements were added in the forms of corresponding oxides.

Analytically pure powders of (NH<sub>4</sub>) H<sub>2</sub>PO<sub>4</sub>, trace element oxides and albite granite powder were mixed by grinding them in an agate mortar for at least 4 h. The mixtures were fused in a platinum crucible in a silicon-molybdenum electric furnace (JGMT-5/180 type) at 1500 °C; fusion time was limited to 1 h to minimize alkali loss, and the melts were quenched in water. In order to generate homogeneous glasses, this process of grinding, fusing, and rapid quenching, was repeated 3 to 4 times for each starting composition. Finally, the glasses were ground to <50 μm for use in experiments. The compositions of the glasses were analyzed by XRF and are shown in Table 1.

## 2.2 Experimental procedure

All runs were conducted in cold-seal Rapid Quenching pressure Vessels (RQV, a kind of “externally heated cold-seal pressure vessel”), using water as the pressure medium for durations of 144 h. The run temperature and pressure were measured by a WRPK-103 type platinum–rhodium thermocouple and Bourdon-tube pressure gauge with errors of 1 °C and 0.05 kbar, respectively. The maximum

temperature gradient at 1 kbar was 5 °C over the 5-cm long capsule, as determined by the calibration of the temperature profile of the tubular electric furnace. The oxygen fugacity (*f*O<sub>2</sub>) of the experimental charge was not directly controlled. The use of GH220 vessels (commensurate to René-41, composed of a Ni-based alloy), coupled with the thermal dissociation of the water pressure medium (2H<sub>2</sub>O = 2H<sub>2</sub> + O<sub>2</sub>) in the vessel, imposes a hydrogen fugacity (by the establishment of osmotic equilibrium between the charge and the pressure buffer within 24 h) equal to the nickel–nickel oxide (NNO) solid-state oxygen fugacity buffer on the experimental charge (Chou 1987; Simon et al. 2005).

About 200 mg of starting glass was loaded into gold capsules, which were 4-mm in outer diameter, 3.8-mm in inner diameter and 50-mm in length. About 200 μl of de-ionized water was injected into the capsule slowly by using a micro-injector to keep the solid–liquid ratio of 1:1. The loaded capsule was immersed in ice water and welded shut by oxy-acetylene flame. The sealed capsule was placed in an oven at 110 °C overnight. After checking for leakage and making sure of no change in mass (<0.5 mg), the capsule was placed inside the cold-seal rapid quenched vessel (RQV), which was inserted into a horizontal tubular electric furnace. The charge was pressurized with water to 0.5 kbar, and then heated to 850 °C in 2–3 h. Then, the pressure was adjusted to the final run pressure of 1.0 kbar. After melting the charge at 850 °C for 24 h, the run temperature was dropped at a rate of 1 °C/min to 800 °C, where the charge was kept for 144 h, in a state that was sufficient to make partitioning experiments in this work

attain equilibrium. At the end of the experiment, the pressure vessel was withdrawn from the tubular heating electric furnace and tilted upwards (at 90° angle from the horizontal). The gold capsule slid into the quenching part of vessel and was then quenched isobarically from 800 °C to ambient-temperature in less than 10 s.

The capsule was removed from the vessel, cleaned with distilled water, examined microscopically and weighed, in order to determine whether the capsule had remained sealed during the run. Only those capsules that showed mechanical integrity and mass loss (<0.5 mg) were processed for analysis. After centrifugation for 30 min, the top end of the capsule was pierced with a stainless steel needle, and the solution was extracted using a syringe. Then the capsule was dried, opened by a razor blade, and boiled in hydrochloric acid for 30 min. After the acid treatment, the sample was rinsed several times with de-ionized water. All of the solutions obtained during these operations were added to the solution withdrawn from the capsule, and then diluted to 5 ml in preparation for analysis. The purpose of the acid treatment is to re-dissolve material precipitated from the fluid during quenching. In this process, the glass does not appear to be significantly affected (Keppler and Wyllie 1991). The quenched silicate melt formed clear, colorless and translucent glass. Sub-microscopic cavities, formed by vapor bubbles, were observed in the appearance of glass. The total volume of these bubbles is estimated at <0.1 vol% of the fluid.

### 2.3 Analysis of experimental products

Chemical composition of the initial glasses was determined by XRF at the State Key Laboratory of Ore Deposit Geochemistry, Institute of Geochemistry, Chinese Academy of Sciences. The major-element composition of the run-product glasses was analyzed by the Shimadzu EMPA-1600 electron microprobe with wavelength dispersive spectrometry (WDS) at the State Key Laboratory of Ore Deposit Geochemistry, Institute of Geochemistry, Chinese Academy of Sciences. Natural Macusite glass was used as standards for the major element, except P, and synthesized P-bearing glass (P<sub>2</sub>O<sub>5</sub> wt% = 2) was used as a standard for P. In order to reduce the loss of alkalis during analysis, the analytical conditions for Na, Al, K and Si were at 20-kV acceleration potential, 2-nA beam current and a 20- $\mu$ m defocused spot. For other major elements the conditions were at 20 kV acceleration potential, 20-nA beam current and a 20- $\mu$ m defocused spot (Morgan and London 1996, 2005). The counting time for all elements was 30 s.

The trace-element concentration in the glasses was measured by LA-ICP-MS (Agilent 7500 Series) at the State Key Laboratory of Continental Dynamics, Northwestern University, Xi'an. It was equipped with a Elan 600DRC

quadrupole mass spectrometer and a 193-nm ArF excimer laser (Geolas200 M laser ablation system). Spots that were petrographically devoid of vapor bubbles were chosen for ablation, and the diameter of the laser ablation beam was set to 30  $\mu$ m. Analysis methods and operating conditions were defined in detail previously (Gao et al. 2002). A US National Institute of Standards and Technology (NIST) standard reference material, NBS-610, was used as the reference silicate glass, and the concentration of Si, determined by EMPA, was used as an internal standard for the quantification of the rare-element concentration in the glasses.

The trace-element concentrations of the aqueous fluids were measured using the solution ICP-MS (Elan 600) at the Isotope Laboratory of Institute of Guangzhou Geochemistry, Chinese Academy of Sciences. Indium (10 bbp in standard solutions) was used as the internal standard for the quantification of REE concentration in the aqueous fluid. According to a number of determined results of standard samples, the relative error of LA-ICP-MS and solution ICP-MS were both less than 10 %.

### 2.4 Sources of experimental error

Much of the error of the partition coefficients comes from the analyses of both the glass and aqueous phases. This error is small if the partition coefficient is less than unity (?) Keppler and Wyllie (1991). With the ICP-MS and LA-ICPMS analyses, the analytical uncertainty is generally <10 %.  $D_i$  represents the ratio of two analyses, so the uncertainty in  $D_i$  is <14 %.

## 3 Experimental results and discussions

### 3.1 The major compositions

It has been determined that the liquidus of the studied initial magmatic systems, which contains 5 wt% H<sub>2</sub>O, ranges from 810 °C at 0.27 wt% P<sub>2</sub>O<sub>5</sub> to 740 °C at 7.71 wt% P<sub>2</sub>O<sub>5</sub>, under a pressure of 1.0 kbar (Tang et al. 2009). The 1:1 ratio of the solid–liquid in the experimental charges makes the experimental systems H<sub>2</sub>O-oversaturated. Thus, it is reasonable to consider that there are only melt and fluid phases in the experimental phase equilibrium systems at 1.0 kbar and 800 °C.

Compared with the corresponding initial glasses (P0T, P2T, P5T and P8T) (Table 1), the main chemical compositions of the run-product glasses (Table 2) have lower content of SiO<sub>2</sub>, Al<sub>2</sub>O<sub>3</sub>, Na<sub>2</sub>O and K<sub>2</sub>O, and no variation of the Fe–Mg components. Microprobe analytical totals for the run-product glasses are in the range of 89.78–94.78 wt%, implying that about 5.22–10.22 wt%

**Table 2** Average chemical compositions of the run-product glasses (melts), determined by EMPA (in wt%)

| Sample                         | P0T   |       |       |       | P2T   |       |       |       | P5T   |       |       |       | P8T   |       |       |       |
|--------------------------------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
|                                | 30–1  | 27–7  | 26–7  | 28–3  | 30–7  | 24–8  | 23–8  | 28–4  | 29–1  | 24–7  | 26–4  | 28–7  | 30–8  | 26–3  | 26–8  | 28–8  |
| P (kbar)                       | 0.5   | 1     | 1     | 1.5   | 0.5   | 1     | 1     | 1.5   | 0.5   | 1     | 1     | 1.5   | 0.5   | 1     | 1     | 1.5   |
| T (°C)                         | 850   | 800   | 850   | 800   | 850   | 800   | 850   | 800   | 850   | 800   | 850   | 800   | 850   | 800   | 850   | 800   |
| SiO <sub>2</sub>               | 70.55 | 69.13 | 68.09 | 67.79 | 69.42 | 66.20 | 67.35 | 66.17 | 66.19 | 64.98 | 65.07 | 66.02 | 64.14 | 65.14 | 64.46 | 62.36 |
| Al <sub>2</sub> O <sub>3</sub> | 15.51 | 14.71 | 14.95 | 15.60 | 14.28 | 14.58 | 14.95 | 14.75 | 14.24 | 14.36 | 14.80 | 14.34 | 14.31 | 14.31 | 14.39 | 14.26 |
| Na <sub>2</sub> O              | 4.19  | 4.00  | 3.95  | 3.61  | 4.13  | 3.30  | 3.72  | 3.58  | 4.04  | 3.78  | 3.88  | 3.53  | 3.50  | 3.50  | 3.55  | 3.31  |
| K <sub>2</sub> O               | 3.56  | 3.25  | 3.38  | 3.18  | 3.12  | 3.06  | 3.13  | 3.22  | 2.86  | 2.98  | 2.81  | 2.81  | 2.73  | 2.73  | 2.80  | 2.73  |
| FeO                            | 0.54  | 0.37  | 0.50  | 0.52  | 0.29  | 0.32  | 0.32  | 0.33  | 0.28  | 0.34  | 0.33  | 0.35  | 0.33  | 0.33  | 0.34  | 0.34  |
| MgO                            | 0.08  | 0.06  | 0.17  | 0.16  | 0.10  | 0.09  | 0.12  | 0.12  | 0.08  | 0.17  | 0.10  | 0.09  | 0.11  | 0.11  | 0.11  | 0.10  |
| MnO                            | 0.09  | 0.07  | 0.07  | 0.07  | 0.06  | 0.07  | 0.06  | 0.06  | 0.06  | 0.07  | 0.06  | 0.06  | 0.06  | 0.06  | 0.07  | 0.06  |
| CaO                            | 0.09  | 0.36  | 0.40  | 0.30  | 0.28  | 0.25  | 0.29  | 0.26  | 0.16  | 0.21  | 0.12  | 0.01  | 0.20  | 0.20  | 0.33  | 0.45  |
| TiO <sub>2</sub>               | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  | 0.00  | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  | 0.01  |
| P <sub>2</sub> O <sub>5</sub>  | 0.17  | 0.18  | 0.23  | 0.20  | 1.42  | 1.38  | 1.34  | 1.28  | 3.34  | 3.68  | 3.50  | 3.40  | 6.19  | 6.09  | 6.01  | 6.20  |
| Total                          | 94.78 | 92.14 | 91.76 | 91.44 | 93.12 | 89.25 | 91.28 | 89.78 | 91.24 | 90.57 | 90.68 | 90.63 | 91.58 | 92.48 | 92.07 | 89.82 |
| ASI                            | 1.43  | 1.37  | 1.38  | 1.57  | 1.35  | 1.59  | 1.50  | 1.51  | 1.42  | 1.46  | 1.54  | 1.62  | 1.58  | 1.58  | 1.52  | 1.56  |

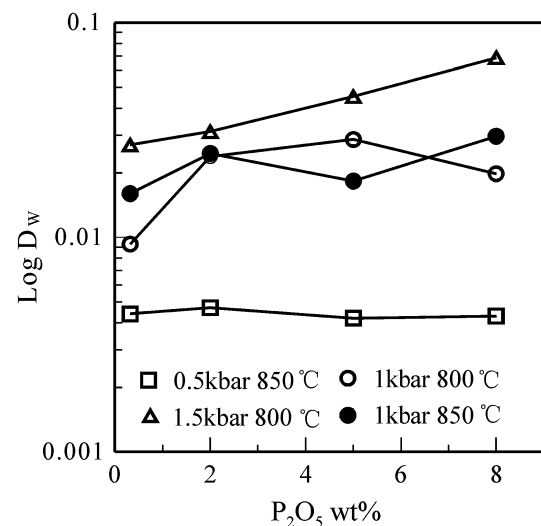
H<sub>2</sub>O was dissolved in the melts. The significant increase of the ASI (Al-saturation index,  $ASI = Al_2O_3 / (Na_2O + K_2O + CaO)$  in mole) indicates that melt-fluid interactions result in more Na, K and Ca partitioning into the fluid phase than Al.

Based on trace element concentrations and masses of the initial, run-product glasses and fluid phase, as well as taking into account 4 wt% solubility of peraluminous melt in aqueous fluid (Webster 1990) and different H<sub>2</sub>O solubility in different run-product glasses (5.22–10.22 wt%), the recovery of trace element can be estimated to be from 85.9 to 98.6 % in all of the runs. The high recovery states that our experimental results in this paper are reliable.

### 3.2 Tungsten

Experimental data for the partitioning of tungsten is shown in Fig. 1 and Table 3. The partition coefficients of tungsten vary from 0.003 to 0.07. According to our experimental results, tungsten fractionates toward the melt.

Phosphate, as a typical ‘hard’ base, was expected to form strong complexes with a ‘hard’ acid like W<sup>6+</sup> (Watson 1976; Ryerson and Hess 1980; Webster et al. 1997). According to London et al. (1993), phosphorus partitions strongly in favor of a silicate melt phase, so the low partition coefficient of W between the P-rich melt and aqueous fluid was expected. However, Keppler (1994) found that the phosphorus content of a coexisting aqueous fluid increases with the total phosphorus content in the melt and with pressure. This result may account for the fact that the vapor/melt partition coefficients of tungsten increase with



**Fig. 1** Partition coefficients of tungsten between aqueous fluid and melt

increasing P<sub>2</sub>O<sub>5</sub> wt% in the melt and increasing pressure (Fig. 1).

The distribution of tungsten between granite melt and the coexisting fluid has been studied extensively (Manning and Henderson 1984; Keppler and Wyllie 1991; Chen and Peng 1994; Zhao et al. 1996; Bai and Koster van Groos 1999). Except for the results of Manning and Henderson (1984), previous studies showed that the capacity of tungsten to dissolve in an aqueous fluid decreases in the following sequence of anions present: Cl, pure H<sub>2</sub>O > CO<sub>2</sub> > F > P. Our data for W contrast with the results

of Manning and Henderson (1984), who found that W fractionates toward the fluid in a P-bearing system ( $D_W = 2.0\text{--}2.7$  at 800 °C and 100 MPa). Though our experiments do not provide any information on the oxidation state of tungsten in the melt and the fluid, we assume  $fO_2$  to be within 2 log units of the NNO buffer (see experimental section). Under these  $fO_2$  conditions, the oxidation state of tungsten is +6. Furthermore, Bai and Koster van Groos (1999) and Chen and Peng (1994) considered that the presence of a small amount of reduced tungsten does not

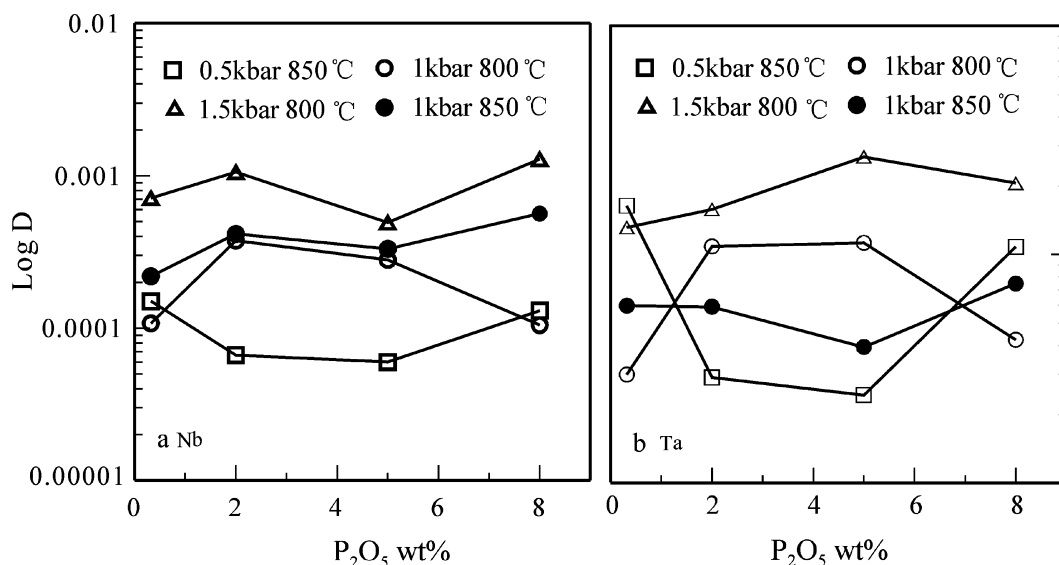
significantly affect its distribution behavior. The differences of  $D_W$  in our work and in the study of Manning and Henderson (1984) are unlikely to be the result of differences in  $fO_2$ , but are more likely to be from differences in fluid composition. The addition of large amounts of  $Na_3PO_4$  made the bulk of their composition peralkaline, and increased the pH of the solution (Urabe 1985). Furthermore, the tungsten concentration (1 wt% W) used by Manning and Henderson (1984) was so high that W could have deviated from Henry's law distribution. In contrast, the

**Table 3** Partition coefficient of W between aqueous fluid and melt

| Run no   | T (°C) | P (Mpa) | $C_{\text{fluid}}$ (ppm) | $C_{\text{melt}}$ (ppm) | D      |
|----------|--------|---------|--------------------------|-------------------------|--------|
| P0T-30-1 | 850    | 50      | 1.74                     | 397.22                  | 0.0044 |
| P0T-27-7 | 800    | 100     | 3.67                     | 394.78                  | 0.0093 |
| P0T-26-7 | 850    | 100     | 6.39                     | 400.42                  | 0.0160 |
| P0T-28-3 | 800    | 150     | 10.91                    | 403.51                  | 0.0270 |
| P2T-30-7 | 850    | 50      | 2.28                     | 481.35                  | 0.0047 |
| P2T-24-8 | 800    | 100     | 10.92                    | 458.99                  | 0.0238 |
| P2T-23-8 | 850    | 100     | 11.60                    | 471.24                  | 0.0246 |
| P2T-28-4 | 800    | 150     | 14.65                    | 469.07                  | 0.0312 |
| P5T-29-1 | 850    | 50      | 2.10                     | 506.35                  | 0.0042 |
| P5T-24-7 | 800    | 100     | 13.41                    | 469.25                  | 0.0286 |
| P5T-26-4 | 850    | 100     | 8.60                     | 471.11                  | 0.0183 |
| P5T-28-7 | 800    | 150     | 21.20                    | 467.31                  | 0.0454 |
| P8T-30-8 | 850    | 50      | 0.70                     | 163.34                  | 0.0043 |
| P8T-26-3 | 800    | 100     | 9.70                     | 489.31                  | 0.0198 |
| P8T-26-8 | 850    | 100     | 14.41                    | 486.50                  | 0.0296 |
| P8T-28-8 | 800    | 150     | 32.63                    | 475.29                  | 0.0687 |

**Table 4** Partition coefficients of Niobium between aqueous fluid and melt

| Run no   | T (°C) | P (kbar) | $C_{\text{fluid}}$ (ppm) | $C_{\text{melt}}$ (ppm) | $D_{\text{fluid/melt}}$ |
|----------|--------|----------|--------------------------|-------------------------|-------------------------|
| P0T-30-1 | 850    | 50       | 0.031                    | 207.43                  | 0.00015                 |
| P0T-27-7 | 800    | 100      | 0.022                    | 203.57                  | 0.00011                 |
| P0T-26-7 | 850    | 100      | 0.046                    | 208.64                  | 0.00022                 |
| P0T-28-3 | 800    | 150      | 0.149                    | 208.51                  | 0.00071                 |
| P2T-30-7 | 850    | 50       | 0.016                    | 236.15                  | 0.00007                 |
| P2T-24-8 | 800    | 100      | 0.085                    | 227.01                  | 0.00037                 |
| P2T-23-8 | 850    | 100      | 0.092                    | 222.33                  | 0.00041                 |
| P2T-28-4 | 800    | 150      | 0.238                    | 224.66                  | 0.00106                 |
| P5T-29-1 | 850    | 50       | 0.017                    | 276.50                  | 0.00006                 |
| P5T-24-7 | 800    | 100      | 0.073                    | 260.76                  | 0.00028                 |
| P5T-26-4 | 850    | 100      | 0.088                    | 265.88                  | 0.00033                 |
| P5T-28-7 | 800    | 150      | 0.128                    | 259.62                  | 0.00049                 |
| P8T-30-8 | 850    | 50       | 0.017                    | 132.54                  | 0.00013                 |
| P8T-26-3 | 800    | 100      | 0.042                    | 397.60                  | 0.00010                 |
| P8T-26-8 | 850    | 100      | 0.220                    | 390.06                  | 0.00056                 |
| P8T-28-8 | 800    | 150      | 0.473                    | 367.58                  | 0.00129                 |



**Fig. 2** Partition coefficients of Niobium and Tantalum between aqueous fluid and melt

**Table 5** Partition coefficients of Tantalum between aqueous fluid and melt

| Run no   | T (°C) | P (kbar) | C <sub>fluid</sub> (ppm) | C <sub>melt</sub> (ppm) | D <sub>fluid/melt</sub> |
|----------|--------|----------|--------------------------|-------------------------|-------------------------|
| P0T-30-1 | 850    | 50       | 0.029                    | 179.30                  | 0.00016                 |
| P0T-27-7 | 800    | 100      | 0.005                    | 170.72                  | 0.00003                 |
| P0T-26-7 | 850    | 100      | 0.011                    | 181.11                  | 0.00006                 |
| P0T-28-3 | 800    | 150      | 0.024                    | 181.08                  | 0.00013                 |
| P2T-30-7 | 850    | 50       | 0.006                    | 216.94                  | 0.00003                 |
| P2T-24-8 | 800    | 100      | 0.023                    | 208.19                  | 0.00011                 |
| P2T-23-8 | 850    | 100      | 0.012                    | 207.00                  | 0.00006                 |
| P2T-28-4 | 800    | 150      | 0.034                    | 217.16                  | 0.00016                 |
| P5T-29-1 | 850    | 50       | 0.005                    | 196.54                  | 0.00002                 |
| P5T-24-7 | 800    | 100      | 0.021                    | 185.76                  | 0.00011                 |
| P5T-26-4 | 850    | 100      | 0.008                    | 194.85                  | 0.00004                 |
| P5T-28-7 | 800    | 150      | 0.054                    | 203.31                  | 0.00027                 |
| P8T-30-8 | 850    | 50       | 0.008                    | 74.63                   | 0.00011                 |
| P8T-26-3 | 800    | 100      | 0.009                    | 223.88                  | 0.00004                 |
| P8T-26-8 | 850    | 100      | 0.017                    | 222.07                  | 0.00007                 |
| P8T-28-8 | 800    | 150      | 0.043                    | 209.78                  | 0.00021                 |

concentrations of W used in our experiments were more geologically relevant.

### 3.3 Niobium and tantalum

The data for  $D_{Nb}$  and  $D_{Ta}$  are shown in Fig. 2, Tables 4 and 5. The distribution behaviors of niobium and tantalum are very similar in our experiments. The partition coefficients of the two elements are very low ( $D_{Nb} = 0.00005\text{--}0.01$  and  $D_{Ta} = 0.00003\text{--}0.002$ ). A change in starting  $P_2O_5$  of the glasses contents between 1.91 and 4.83 wt% has no significant effect on  $D_{Nb}$  and  $D_{Ta}$ . But as the pressure increases, both  $D_{Nb}$  and  $D_{Ta}$  increase.

In previous studies,  $D_{Nb}$  varied 1–3 orders of magnitude. Webster et al. (1989) found  $D_{Nb}$  to be affected by pressure, temperature and fluid composition for F-enriched topaz rhyolite melt. At pressure = 4.0 kbar, Nb partitions into the melt, with the partitioning being apparently independent of temperature. As the pressure decreases, Nb partitions in favor of the fluid and  $D_{Nb}$  increase with temperature. As the mole fraction of water in the fluid increases, Nb partitions increasingly in favor of the fluid. Our  $D_{Nb}$  is similar to the values found by London et al. (1988) and Zhao et al. (1996) (0–0.1 and 0.0019–0.081 respectively), although their  $D_{Nb}$  is higher than ours. Zhao et al. (1996) determined  $D_{Ta} = 0.0023\text{--}0.089$ . The differences between the results we obtained and previous studies are likely mainly attributed to the difference in fluid composition and melt.

## 4 Conclusions

Relative to the coexisting aqueous fluid, W, Nb and Ta partition in favor of P-rich peraluminous granitic melt at 800–850 °C and 50–150 MPa. The ranges of the fluid/melt partition coefficients of W, Nb and Ta are: 0.003–0.07, 0.00005–0.001, 0.00003–0.0002, respectively.  $D_W$ ,  $D_{Nb}$ , and  $D_{Ta}$  are all affected by pressure, but there is no evidence of an effect of  $P_2O_5$  on these elements, except for W.

The  $D_W$  is less than 0.01; therefore it is difficult to derive a W-enriched fluid from a P-rich peraluminous melt system, especially when phosphorus is the only complexing agent. Our results also show that Nb and Ta tend to distribute in the melt when it is in the magmatic-hydrothermal stage. In the late period of crystallization of magma, Nb and Ta will form discrete independent minerals like tantalite and columbite.

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